

software age

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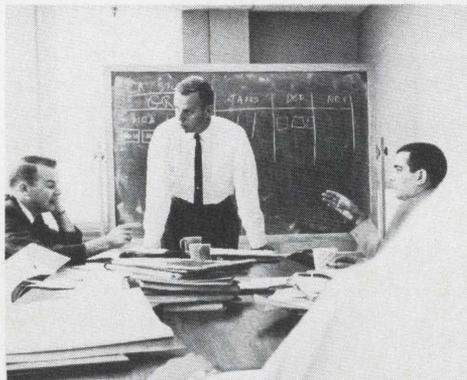
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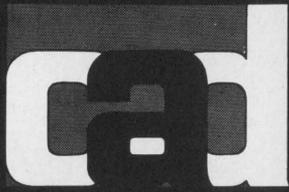
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# software age

OCTOBER, 1968

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## new products

A major new proprietary software package that will enable managers of medium-sized data processing installations to improve day-by-day scheduling, planning and control of personnel and machine time was announced by Brandon Applied Systems, Inc. The package, the Resource Management System (RMS), consists of two subsystems: one for operations control, the other for project control.

RMS is designed to be compiled and run on a minimum 65K IBM 360/30, under DOS. The system is written in COBOL E, with certain routines in ALP where technical factors preclude COBOL. Equipment scheduling can be done for any machine or combination of machines; each is considered as a work station, with qualitative and quantitative attributes. Multi-processing environments are treated as multiple work stations. Interface with OS-360 can be provided for input data and scheduling purposes.

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The Graphic Systems Division of Computer Industries Inc. has announced the development of a new digital plotting system operating from punched paper tape. The new system will be marketed as the PTD (Punched Paper Tape Delta Incremental Plotting System). Among the applications of the new PTD are the plotting of engineering variables from time-shared computers at a remote terminal, verification of tapes for numerical control machine tools.

Special features of the PTD include multiple-step programming, which allows

up to 127 incremental steps in either of two two-dimensional directions from a single input command. This type of programming allows the plotter to be driven from paper tape supplied by a teletype, and is ideal for remote-terminal graphics, permitting data to be transmitted in delta format, affording significant savings in computer and transmission time. The system employs either a low-cost 12-inch plotter or a more flexible 30-inch plotter.

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\* \* \*

An engineer, scientist or any one who uses complicated mathematics can now carry a lightweight computer/calculator keyboard to any location, dial into a central computing station from a standard telephone and perform his calculations. System has been introduced by the Mathatronics Division of Barry Wright Corporation, and marketed by the company's Wright Line Division.



The new system uses an acoustical coupler which sends and receives tone signals through a standard telephone receiver.

To operate the system dial the number of the central computing station, place the telephone receiver in a special nest on the keyboard unit and enter problems.

The system also has a number memory that will store up to eight constants, and a formula memory that allows it to learn and automatically work complex formulas.

If desired, the keyboard units may be directly wired to the central station, or can even be operated by means of a two-way radio hook up.

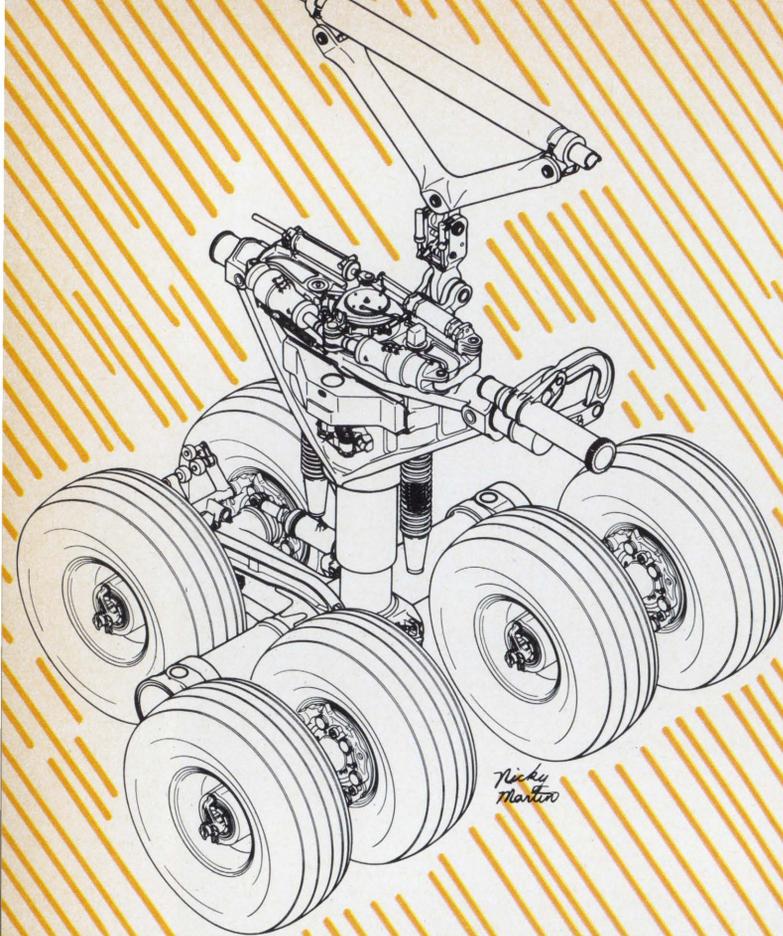
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\* \* \*

Scientific Data Systems has developed a time sharing software system for its Sigma 5 computer, thus adding simultaneous time sharing to the Sigma 5's batch processing

(Continued on page 30)





*Norman S. Currey*

*Aircraft Design Engineer Specialist, Advanced Design,  
Lockheed-Georgia Co.*

■ The C-5 landing gear was probably the first landing gear developed by a form of computer-aided design. The sophistication of present-day techniques had not been established at the time of the C-5 study phase, but the various parameters and processes were quite similar.

Prior to the C-5 era, the selection of an airplane's landing gear configuration was a fairly elementary process. There would be two shock struts for the main gear and one for the nose gear. The strut loads were statically determinate, and it was a simple matter to determine tire loads. These loads depended upon how many tires were used, and this was to a great extent a matter of space availability in the landing gear housing. Except in rare cases, there were always one, two or four tires per main gear shock strut, and these were arranged in simple, con-

ventional patterns. Such parameters as flotation (the ability of an airplane to land on a given runway a specified number of times before runway break-up), maintainability, reliability, bump capability and kneeling capability were rarely if ever considered as contractual requirements.

Then came the C-5, and to understand the necessity for sophisticated landing gear selection, it is necessary to review some of the design and operational philosophy of that airplane.

The C-5 is the largest aircraft in the world, with a normal design gross weight of 728,000 pounds. It is about twice as heavy as present heavy transport aircraft, and yet it must be able to operate on the same runways as those aircraft. At a somewhat lighter weight it must be able to operate on bare soil or matted runways, and these surfaces by definition could have a roughness equivalent to 3-inch high step bumps or severe waviness.

A fleet of C-5's can transport a fully-equipped infantry division anywhere in the world, utilizing air strips at which there are few maintenance facilities and a minimum of ground support equipment for loading and unloading the aircraft.

These requirements necessitated a high flotation landing gear to prevent conventional runway break-up at maximum weight, and to permit soft runway operation. The gear had to be designed to traverse substantial airfield roughness such that airframe structural effects were minimized. Maintenance facilities being minimal at remote air strips, the gear had to require little maintenance and had to have high reliability, and in order to eliminate the need for elaborate docks, the gear had to incorporate a device to lower the fuselage close to the ground—this is referred to as a kneeling capability. It was considered that the C-5 would have to land in high cross-wind conditions, so it was required that the gear be able to rotate left and right of neutral to permit such landings. In this case, the landing gear travels straight down the runway while the fuselage remains vectored into wind

# Computer Aided Design

## -5A Main Landing Gear

by as much as 20 degrees to the runway centerline.

Lockheed guaranteed these capabilities as a part of the contract, and also guaranteed the airplane weight. So despite the fact that the landing gear had to incorporate far more features than any previous gear, it also had to have minimum weight—a combination which provided an unparalleled engineering challenge to the designers of the C-5.

### Parametric Study

In determining an optimum C-5 airlifter configuration, three gross weight variants were considered by Lockheed-Georgia for early sub-optimization of the landing gear. These variants had gross weights of 550,000, 650,000 and 750,000 pounds respectively. A parametric study was conducted to define the optimal landing gear for any of these configurations. Study results were fed back and became part of an over-all design and size determination analysis.

During the course of the study, some 660 individual main landing gear configurations were evaluated for each of the three gross weights under consideration. These configurations included three different types of installation and six different bogie shapes. Figure 1 shows the installation types—wing-mounted, under-

floor-mounted, and side fuselage-mounted gears. The wing-mounted gear transmits loads directly into the wing structure, permitting a simpler and more efficient fuselage structural design. Under some circumstances, suitably-faired wing pods may enhance aerodynamic characteristics of the wing by improving over-all cross section area distribution.

The underfloor mounting permits a minimum number of wheels in tandem and may obviate the need for main gear steering, resulting in a simpler and more reliable design.

The side fuselage-mounted gear has the advantage of simpler pod fairings and gear door installation in addition to having less effect on underfloor structural design.

The six bogie types are shown in Figure 2. They all have advantages and disadvantages in specific applications. For instance, Type 3 proved to be the most suitable for the underfloor gear, while Type 5 was the best for a side fuselage mounting. A wing-mounted gear would probably take advantage of the smaller tire sizes afforded by Type 4.

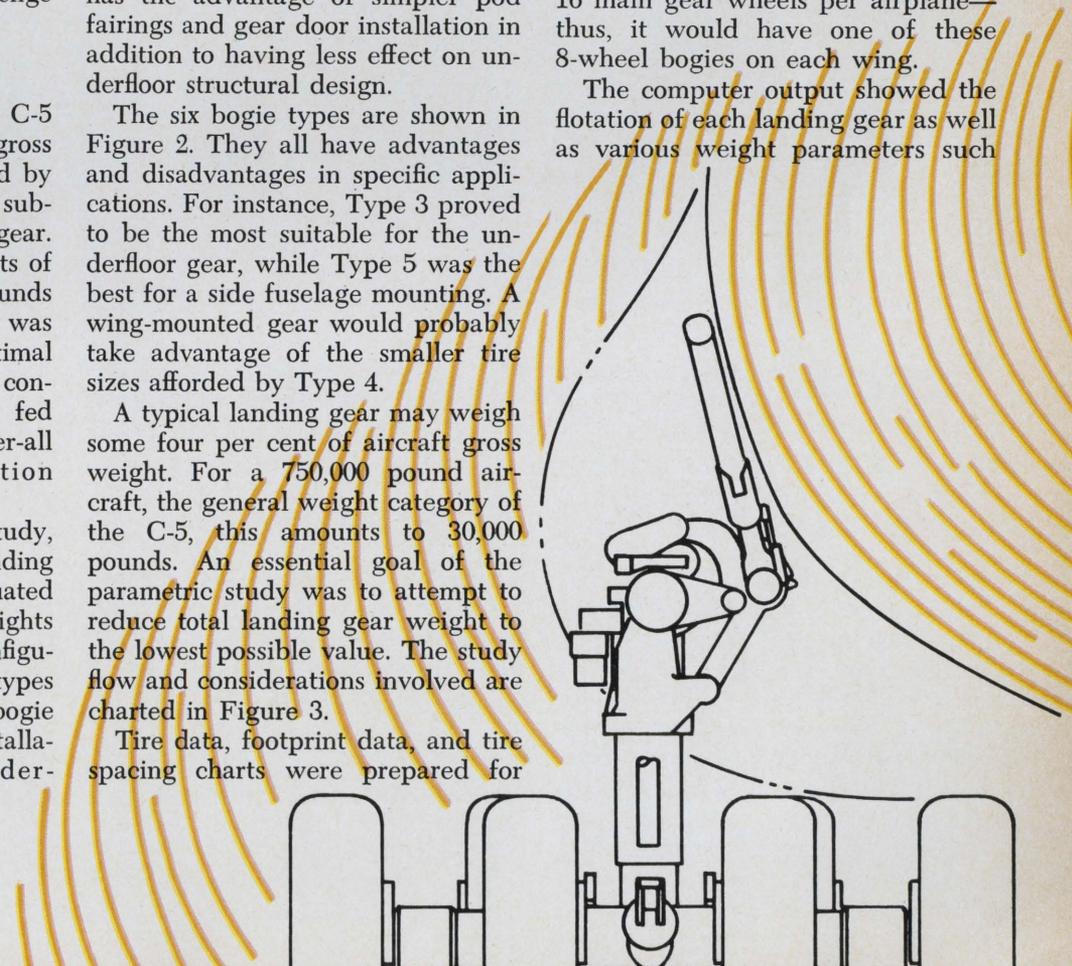
A typical landing gear may weigh some four per cent of aircraft gross weight. For a 750,000 pound aircraft, this amounts to 30,000 pounds. An essential goal of the parametric study was to attempt to reduce total landing gear weight to the lowest possible value. The study flow and considerations involved are charted in Figure 3.

Tire data, footprint data, and tire spacing charts were prepared for

analysis prior to initiation of landing gear design. A matrix of pod fairing shapes was established and, from this, wetted areas were established for each gear variant being considered. Thus, for any given bogie configuration, the wetted area changed whenever a tire size was changed—unless the tire was so small that it was housed entirely within the natural contour of the fuselage. Weight calculations for each landing gear design, along with pod and flotation data were fed into a digital computer.

Each landing gear variant was appropriately coded for easy identification. An A-4-16 gear for instance would be wing-mounted (type A), having a type 4 bogie, and a total of 16 main gear wheels per airplane—thus, it would have one of these 8-wheel bogies on each wing.

The computer output showed the flotation of each landing gear as well as various weight parameters such



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as landing gear weight, fuselage or wing weight change, and effect on take-off gross weight. This output was put through a sorting process which listed all gears in order of flotation, weight, and weight/flotation. The best of 2600 landing gear variants were selected from this assortment for each gross weight design. A second screening further evaluated kneeling capability, practicability, and rough field capability to produce a final listing for selection of the optimal main landing gear for the C-5.

The nose landing gear was omitted from this study. It was obvious at the outset that this would be fairly conventional, and its only effect would be to modify the flotation values. After the main gear had been selected, the nose gear flotation effect was calculated for that particular gear.

**Tires**

Tires must have adequate static load rating, minimum size for stowage, maximum contact area for flotation, minimum weight, a wheel

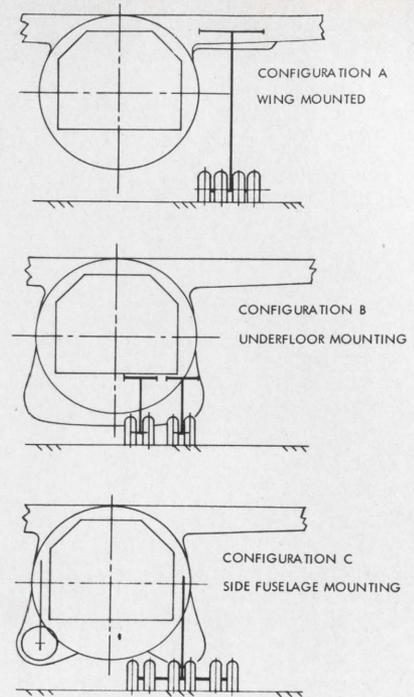


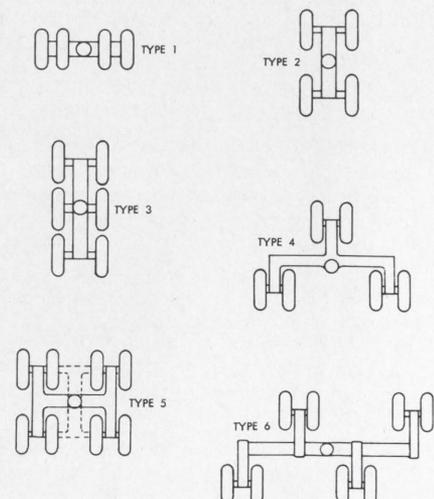
Fig. 1. Installation Types

diameter consistent with brake requirements, and a section height large enough to "swallow" the bumps on the airfield.

It is evident that an incompatibility exists between these factors. A smaller tire is better for minimum stowage space, and minimum weight. A large tire is better for contact area, load capacity and, as it usually has a larger wheel, it is then better for brake installation. For maximum bump capability a large tire on a small wheel is best.

The ultimate tire selection is one of the most important factors in choosing an optimum landing gear. Consequently, 27 tires, all having

Fig. 2. Bogie Types



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adequate load rating, were considered in the parametric study.

As indicated in Figure 4, an approximate logarithmic increase in flotation is achieved with a reduction in tire load, a coverage being defined as a sufficient number of passes to completely cover the runway traffic lane one time with adjacent tire tracks.

Tire load can be decreased by increasing the number of wheels. The greater the number of wheels, however, the more difficult it is to avoid

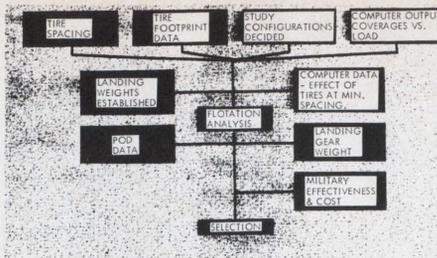


Fig. 3. Method for Flotation Evaluation

wheels tracking one behind the other, thereby limiting load distribution over the terrain. Besides degra-

dations in reliability, maintainability, cost, weight and stowage capabilities, increasing the number of wheels requires a larger pod fairing, adding to the aircraft drag. Keeping these factors in mind, main landing gears with 8, 12, 16, 18, 24 and 32 wheels were considered as configurations during the course of the study.

Measured contact areas applicable to 35 per cent tire deflection were used as study criteria. No attempt was made to evaluate pressures needed to withstand operational loading conditions for each tire size. This would have involved checking load distributions among tires for all



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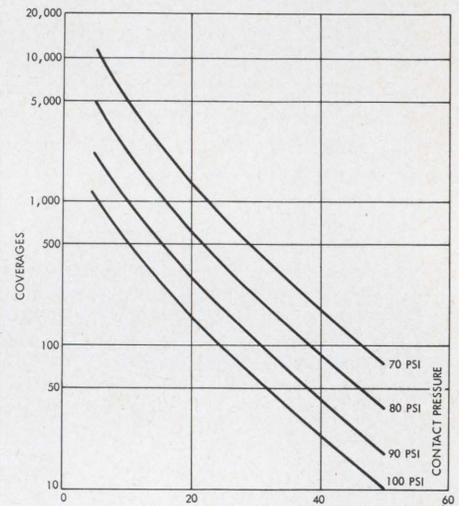


Fig. 4. Flotation vs. Tire Load and Pressure

bogie configurations, with and without flat tires, for standard and sub-standard airfields, and under all loading conditions such as braked turn, steady turn and 2g taxi operation. For the purposes of the study, there was very little to be gained from making such calculations.

Figure 5 shows the tire footprint data used in the analysis. The columns show some of the parameters used in calculating flotation. At that time, the flotation criteria indicated that there would be no interaction between tires spaced 4R or more apart, where R is the radius of the circle equivalent to the contact area. A column is provided, therefore, to show the minimum tire spacing for optimum flotation.

### Tire Spacing

Among all the various bogie configurations, there were cases where 4R tire spacing could not be used, and there were other cases, such as

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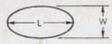
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Tire Type	Tire	Contact Area	A/π	√A	R	W	L	4R	80-W	.75W
III	13.50 - 16	181.5	57.8	13.47	7.60	11.77	19.63	30.40	91.77	8.83
	15.00 - 16	219	69.7	14.80	8.35	12.94	21.56	33.40	92.94	9.71
	16.00 - 16	244	77.7	15.62	8.81	13.65	22.76	35.24	93.65	10.24
	17.00 - 16	268.5	85.5	16.38	9.24	14.32	23.87	36.96	94.32	10.74
	15.50 - 20	230	73.2	15.16	8.55	13.25	22.09	34.20	93.25	9.94
	15.50 - 18	244	77.7	15.62	8.81	13.65	22.76	35.24	93.65	10.24
	17.00 - 20	264	84.0	16.25	9.17	14.20	23.68	36.68	94.20	10.65
	20.00 - 20	382	121.6	19.54	11.02	17.08	28.47	44.08	97.08	12.81
	19.00 - 23	330	105.0	18.16	10.24	15.87	26.46	40.96	95.87	11.90
	25.00 - 28	526	167.3	22.94	12.94	20.05	33.42	51.76	100.05	15.04
VII	30 x 7.7	68	21.6	8.25	4.65	7.21	12.02	18.60	87.21	5.41
	30 x 8.8	88	28.0	9.38	5.29	8.20	13.67	21.16	88.20	6.15
	46 x 9	115	36.6	10.73	6.05	9.38	15.63	24.20	89.38	7.04
	36 x 11	120	38.2	10.96	6.18	9.58	15.97	24.72	89.58	7.19
	38 x 11	126	40.1	11.22	6.33	9.81	16.35	25.32	89.81	7.36
	40 x 12	163	51.9	12.77	7.20	11.16	18.61	28.80	91.16	8.37
	39 x 13	147	46.8	12.12	6.84	10.59	17.66	27.36	90.59	7.94
	44 x 13	203	64.6	14.25	8.04	12.45	20.76	32.16	92.45	9.34
	40 x 14	183	58.2	13.56	7.65	11.85	19.76	30.60	91.85	8.89
	44 x 16	219	69.7	14.80	8.35	12.94	21.56	33.40	92.94	9.71
	46 x 16	220	70.0	14.83	8.36	12.96	21.61	33.44	92.96	9.72
	56 x 16	278	88.5	16.67	9.40	14.57	24.29	37.60	94.57	10.93
	49 x 17	261	83.1	16.15	9.11	14.12	23.53	36.44	94.12	10.59
VIII	41 x 15.0-18	186	59.2	13.64	7.69	11.92	19.87	30.76	91.92	8.94
	50 x 20.0-20	276	87.5	16.58	9.35	14.49	24.16	37.40	94.49	10.87
	45 x 24 - 16	307	97.7	17.52	9.88	15.31	25.53	39.52	95.31	11.48
	56 x 30 - 15	603	192.0	24.56	13.85	21.47	35.78	55.00	101.47	16.10

Fig. 5. Tire Footprint Data

four tires side-by-side on one axle, where it was of interest to learn the effect of close tire spacing. An empirical formula was developed to ascertain minimum spacing when two tires are mounted on one wheel, as with the B-58 Hustler, or with wheels very close together. This showed:

Where:

$$S_{min} = 0.40 (2H_t + W_t + W_f)$$

$$S_{min} = \text{Minimum tire spacing}$$

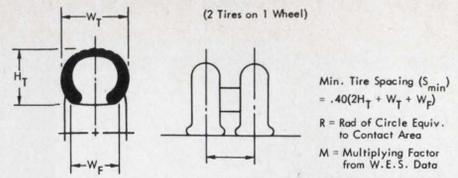
$H_t$  = Tire section height  
 $W_t$  = Tire section width  
 $W_f$  = Width between wheel flanges.

Results of this formula were tabulated for various tire types and sizes with two tires on one wheel, and for a bogie beam located between wheels. Figure 6 shows the tabulation for two tires on one wheel.

### Computer Data

Charts were prepared for each of the permutations of the 660 configurations investigated. In order to develop these charts, the flotation was calculated for each case, the weight of the gear was evaluated, and pod and drag effects were determined. Then, for each configuration, tire size and gross weight, the following data was supplied to the computer:

- Structure weight (pod + airframe structure effect)
- Landing gear weight.
- Wetted area increase due to pod (S)
- Flotation
- Factor  $K_1$ —see below
- Factor  $K_2$ —see below



Tire Type	Tire	$S_{min}$	R	S/R	$M_{max}$	$S_{op max}$	$M_{min}$
III	13.50 - 16	19.52	7.60	2.57	1.36	30.40	1.0
	15.00 - 16	21.18	8.35	2.54	1.365	33.40	1.0
	16.00 - 16	22.18	8.81	2.52	1.37	35.24	1.0
	17.00 - 16	23.88	9.24	2.58	1.355	36.96	1.0
	15.50 - 20	21.80	8.55	2.55	1.363	34.20	1.0
	15.50 - 18*	22.60	8.81	2.57	1.36	35.24	1.0
	17.00 - 20	23.70	9.17	2.58	1.355	36.68	1.0
	20.00 - 20	28.64	11.02	2.60	1.35	44.08	1.0
	19.00 - 23	26.49	10.24	2.59	1.355	40.96	1.0
	25.00 - 28	35.34	12.94	2.73	1.319	51.76	1.0
VII	30 x 7.7	10.90	4.65	2.34	1.416	18.60	1.0
	30 x 8.8	12.52	5.29	2.37	1.408	21.16	1.0
	46 x 9	12.44	6.05	2.06	1.485	24.20	1.0
	36 x 11	15.84	6.18	2.56	1.362	24.72	1.0
	38 x 11	15.84	6.33	2.50	1.377	25.32	1.0
	40 x 12	17.62	7.20	2.45	1.388	28.80	1.0
	39 x 13	18.10	6.84	2.65	1.339	27.36	1.0
	44 x 13	19.22	8.04	2.39	1.403	32.16	1.0
	40 x 14	19.52	7.65	2.55	1.363	30.60	1.0
	44 x 16	21.80	8.35	2.61	1.348	33.40	1.0
	46 x 16	21.80	8.36	2.61	1.348	33.44	1.0
	56 x 16	22.94	9.40	2.44	1.390	37.60	1.0
	49 x 17	23.70	9.11	2.60	1.352	36.44	1.0
VIII	41 x 15.0 - 18	20.30	7.69	2.64	1.341	30.76	1.0
	50 x 20.0 - 20	26.50	9.35	2.83	1.293	37.40	1.0
	45 x 24 - 16*	29.40	9.88	2.98	1.256	39.52	1.0
	56 x 30 - 15*	38.30	13.85	2.77	1.308	55.40	1.0

Fig. 6. Tire Spacing

In the aerodynamic evaluation of the pods, it was recognized that each pod would have different drag characteristics, and by holding a constant payload-range capability for

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each airplane weight, the pod drag can be interpreted as a change in take-off gross weight. In other words, a high drag pod will necessitate additional fuel to meet that payload-range capability, and this additional fuel is reflected in increased take-off weight. Thus  $K_1$  is a factor predicated upon statistical and wind tunnel data, differing for each weight and pod type considered. The value of  $K_1$  for a side fuselage-mounted gear varied from 10.8 for a 550,000 pound airplane to 16.9 for a 750,000 pound airplane, and the change in take-off weight due to pod drag was given by

$$\Delta \text{TOGW} = K_1 \times S_w$$

where  $S_w$  is the difference between the pod wetted area and the wetted area of the fuselage or wing covered by that pod.

Factor  $K_2$  reflects the effect of incremental weight changes on take-off gross weight at a constant wing loading and thrust loading. Thus, increasing the diameter of a tire increases the weight of the gear, and this results in an airplane weight increase of  $K_2W$ , where  $W$  is the structure weight plus gear weight.

The value of  $K_2$  did not change with landing gear type, and varied from 3.0 for 550,000 pound airplanes to 3.9 for 750,000 pound airplanes.

Thus, the weight effect was recognized in total by the following equation:

$$\Delta \text{TOGW} = (K_1 \times S_w) + (K_2 \times W)$$

For wing-mounted gears this equation was further extended to include the effects of flap span reduction.

Flotation data was calculated for both optimum and minimum tire spacing for each configuration being considered, and the methods used are given in AFSCM 80-1—Handbook of Instructions for Aircraft Designers.

#### Inflight Tire Deflation

The computer analysis also showed the effects of using inflight tire deflation. This is a system which deflates the tires in flight such that the tires are at their optimum deflection at landing, just as they were at take-off. Take-off tire pressure is predicated upon take-off weight. During flight, weight is reduced due to fuel usage, and when the airplane lands its required tire pressure may

well be considerably less than it was at take-off. Flotation is improved whenever tire pressure is reduced, and the inflight tire deflation system provides this reduction. However, any additional system has a cost, weight, maintainability and reliability impact, so the merits of such a system were evaluated as part of this study.

#### Computer Analysis

One set of charts was prepared showing all the data pertaining to

each specific landing gear configuration. For instance, under the heading of a C-4-24 gear—a side fuselage-mounted gear with a type 4 bogie and 24 main gear wheels per aircraft—the chart showed the flotation and weight effect for each of the 17 possible tire sizes, with and without inflight tire deflation, at optimum and minimum tire spacing for each of the three gross weights considered.

Computer data then sorted out all the gears so that one sheet showed them in order of weight, one sheet



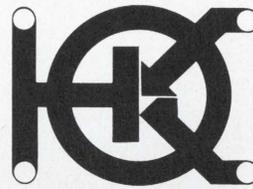
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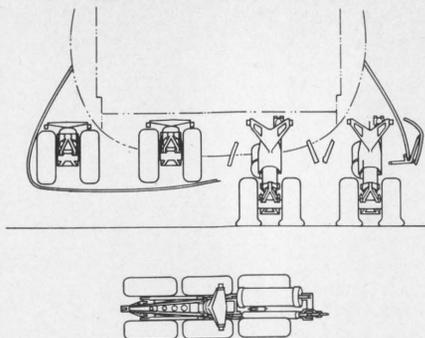


Fig. 7. Underflows Landing Gear

showed them in order of flotation, and a third sheet showed them in order of flotation per pound of weight. Thus, one gear may have indicated that it had extremely high flotation, but unless its weight was compatible, it would not necessarily be a choice gear.

An operational analysis had been conducted concurrently with the parametric study which showed the flotation that the airplane should have for each gross weight. For instance, it was shown that a 550,000 pound airplane would have far better flotation than the 750,000 pound airplane, as more of the "light" airplanes would be required to land at a given field in order to land a specific total load. The precise flotation values were determined by mission analysis, and these showed which landing gears were best suited for the particular airplanes.

For each airplane weight a graph was plotted which showed how all the "best" gears related to each other in terms of airplane gross weight and flotation. Knowing what the flotation value should be for that weight, it was then possible to select the best main landing gears for each of the three gross weights. In the graphical analysis there were 184 chosen gears, and from this 28 were chosen for final screening.

#### Landing Gear Selection

The final selection did not involve any computer operation. It was, rather, a logic analysis. The initial studies had shown that the airplane should have a kneeling capability to lower the cargo floor such that the lower fuselage was very close to the ground. If any of the selected gears were not capable of providing this capability then they were eliminated. For instance, an underfloor gear with

large 56 x 16 size tires would not be able to provide this feature because of the large tire diameter situated between the cargo floor and the ground.

Various aspects of practicability were then considered, and if a particular arrangement did not appear too practical it was eliminated. A typical case would be four large tires side-by-side at optimum spacing. Such a design would lead to severe axle design and braking problems.

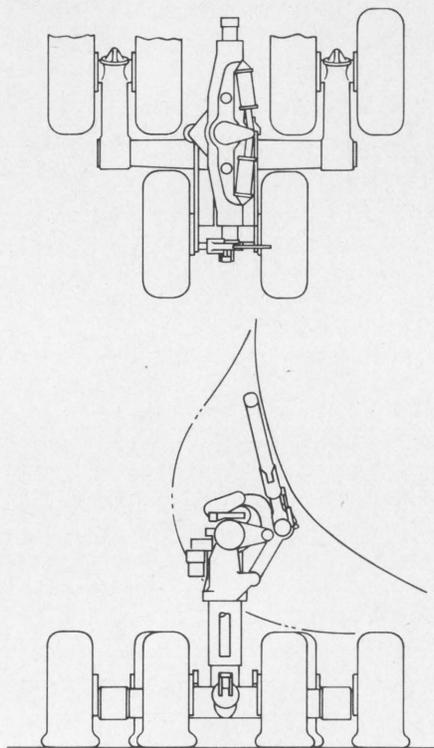


Fig. 8. Selected Main Landing Gear

The tires of the select gears were then evaluated for bump capability, and at that time a six-inch bump height was used as the criteria. To "swallow" such a bump, the tire had to have six inches between its normal loaded radius and its flat tire radius. If such a capability was not available then that gear was rejected.

Any of the remaining gear configurations having a high weight-to-flotation ratio were eliminated, and this left nine gears for final evaluation.

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A maintenance, reliability and cost analysis was made on these gears, and from this two configurations emerged as the most suitable main landing gears for the C-5. They were the present twin tricycle arrangement, using a Type 5 bogie mounted on the side of the fuselage, and an underfloor arrangement using a type 3 bogie and having 24 main gear wheels.

The underfloor arrangement is shown in Figure 7. It was believed that main gear steering would not be required with such an arrangement. The retraction method was relatively simple in that the shock strut merely rotated fore and aft. In addition, the bogie was relatively light due to minimization of torsional loads. A comparison of the two competing designs revealed, however, that the underfloor-mounted gear incurred extremely severe door problems and had less flotation than the finally-selected side-fuselage-mounted design.

#### Finally-Selected Main Landing Gear

A diagram of the finally-selected six-wheel bogie and tire arrangement is presented in Figure 8. Other details of the gear can be seen in Figure 9. The mechanism required for crosswind positioning is located at the top of the gear. It rotates the bogie up to 20 degrees left and right of neutral depending upon the magnitude of the crosswind during landing.

The kneeling system is shown in Figure 10. The main gear is suspended from the fuselage main frames at two trunnion points. These two trunnions are part of a large aluminum alloy yoke forging. The shock strut is free to slide up and down through a hole in the center of the forging. The top of the shock strut terminates in a T-shaped crosshead. Ballscrews are suspended from the crosshead and pass through ballnuts housed inside the yoke. By rotating the ballnuts, the crosshead is separated from the yoke and the yoke slides downward around the shock strut until it bottoms out on the bogie beam.

A chain drive connected to an air motor, powered by engine bleed air drives the ballnuts within the yoke. The system can be braked to a stop at any point of travel desired.

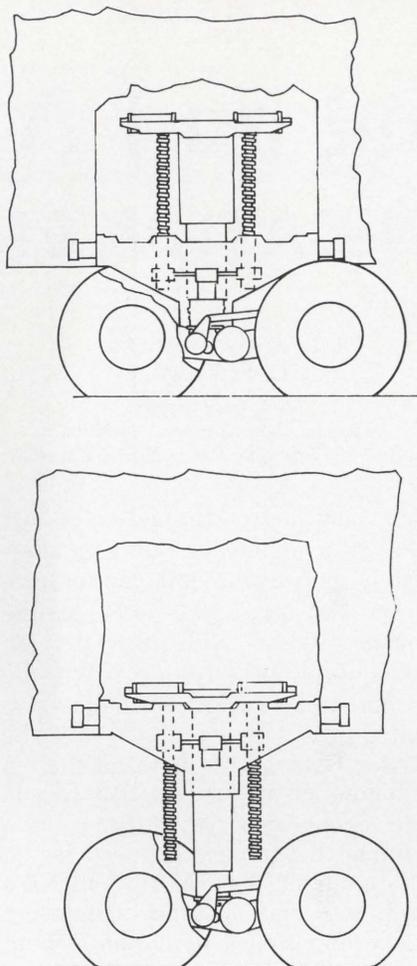


Fig. 10. Kneeling System

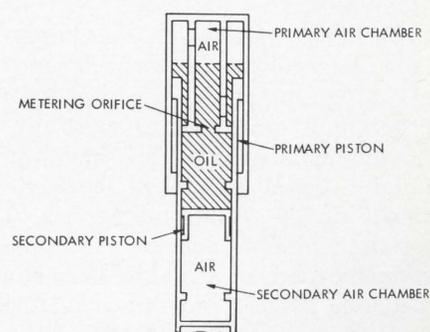
To retract the landing gear, a rotation cylinder on the top of the crosshead rotates the strut and bogie through 90 degrees so that the forward wheels are facing the aircraft centerline. The landing gear is then swung about its trunnion points until it reaches its retracted position beneath the cargo floor.

The shock strut is a unique double-acting design in which there are two chambers instead of one. As shown in Figure 11, it has a primary chamber which acts in the same way as a conventional shock strut. But at the base of that chamber there is a secondary piston which floats at the top of an air-charged secondary chamber. This chamber is preloaded by compressed air in excess of maximum static requirements, and when the landing gear encounters airfield roughness this secondary chamber acts in the same way as a hydraulic surge damper, absorbing unsprung mass momentum and attenuating peak loads. In this way the loads which would be transmitted to the airframe structure are greatly reduced.

At the base of the shock strut—where it attaches to the bogie—there is a universal joint. This permits the bogie to rotate in any plane as it traverses roughness, ensuring that all three wheel pairs of that bogie are always in contact with the ground for optimum load distribution.

In summary, the C-5 landing gear has undergone a long and rigorous development. With its 24 main gear wheels, arranged in an optimum pattern, it can operate at maximum gross weight on the same runways as present-day jets which are less than half the weight of the C-5. At a reduced weight it can make more than a hundred landings and take-offs from a bare soil field. With close attention having been paid to detail design it is predicted that it will meet its stringent maintainability guarantees, and this, together with its kneeling system, will minimize the amount of equipment required to support the airplane at remote bases. One interesting feature of the kneeling system is that it is possible to kneel individual main gears. In this case, instead of the fuselage being lowered, one gear is raised, with the other three gears supporting the airplane. This obviates the necessity for jacking to accomplish routine landing gear maintenance—a feature which paid off during taxi tests when a tire blew. The affected gear was raised clear of the ground and the airplane taxied back to the hangar for a tire change. It is also of interest to report that the test pilots have found the airplane extremely easy to handle on the ground, despite its tremendous size and its 24 main gear wheels. One indication of this is the fact that it has turned 180 degrees in 112 feet width of runway—well within its guarantee. ■

Fig. 11. Double-Acting Shock Strut



# Scheduling and Allocating

## -IN A COMMUNICATION ENVIRONMENT-

L. J. Endicott, Jr.

L. S. Kreger

IBM Corporation  
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Research Triangle Park, North Carolina

■ The primary purpose of systems programming has always been to provide general programs which can be used by many users, to avoid having everyone code the same routines. It is still an important purpose. Today, however, there is an additional, more pressing reason for system programs: to guide the user in fully utilizing all of the system's resources—both software and hardware—at his disposal. Guidance can be provided through the structure of the language and the allocation of resources.

Allocation of resources includes scheduling, which in a priority system occurs at the time a priority is established. Scheduling must not be confused with dispatching, which is a simple queue-management function. Scheduling includes: *what* gets on the dispatcher's queue, *how* it gets on the queue, *when* it gets on the queue, and where it goes into the queue.

Allocation may be static or dynamic. Static allocation is predetermined and fixed by the application program for a specific application. There is no allocation manager to assign resources. Dynamic allocation occurs when resources allocations—including CPU time—are made or changed during program execution.

This "rate of change" is an important determinant of the efficiency of a program and varies widely from program to program. In most programming, resources are not optimally shared because of the inefficiency of the sharing mechanism. A resource might not be available when needed, or it might be made available when a program is unable to use it. Physical resource allocation

may be performed once per IPL, or assignments may pass alternately between a job control program and successive jobs. Assignments may be made once per job step, or physical resources may be assigned to a region during job-step initialization, which then can be passed from one task to another in a hierarchy of tasks in that region. The more resources existing in a system, the greater the need for an allocation mechanism that allows a high rate of change in assignment while imposing a minimum amount of overhead.

A mechanism has been designed, as part of the Queued Telecommunications Access Method (QTAM), which allows a high rate of change of resource allocation, and an external language which can be modified by the user. (This is an IBM Type I Program, available in Operating System/360 and Disk Operating System/360.) The language is structured from several types of delimited macros. The user is shown what types are to be used in which construction of his program—guiding him in the construction of his program. These facilities aid the user to achieve maximum utilization of his total system's resources. Although QTAM was developed for scheduling and allocating of communication systems, its principles are applicable to any control program. However, it was designed with the special requirements of a Tele-processing environment in mind.

### The Tele-Processing Environment

Tele-processing—data communication—I/O is not generically different from tape or disk I/O; its dif-

ferences are in degree rather than in kind. The need for dynamic allocation with a high rate of change results from the peculiarities of a Tele-processing environment. Among these are:

**Slower Data Rate**—The transmission rate for the IBM 1050 Data Communications System, for example, is just under 15 characters per second. At this rate, it becomes intolerable to tie up a full record area for the entire time it takes to read a complete message. A 400-character record will require more than 26 seconds to read in after the first character has been received. If only half of the space were made available for only half of the time, over 5,000 200-character records conceivably could be read and processed from our fastest tape drives.

**Greater Number of I/O Channels**—A 100-line system is not considered impossible in a Tele-processing environment. A 100-line system with an average of five terminals on a line and five I/O components per terminal would amount to an admittedly quite large system of 2,500 I/O devices. Exceptional, perhaps, but not impossible.

**Higher Error Rate**—Error rates of only one in several million characters are achievable with tapes or disks. However, because of the long transmission lines, etc., one transmission error in 5,000 characters may be considered quite acceptable in some Tele-processing applications. Further, these are usually more critical than in telephone and teletype transmissions where the meaning in context often neutralizes errors.

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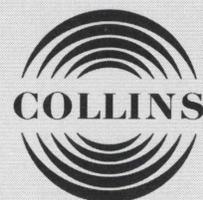
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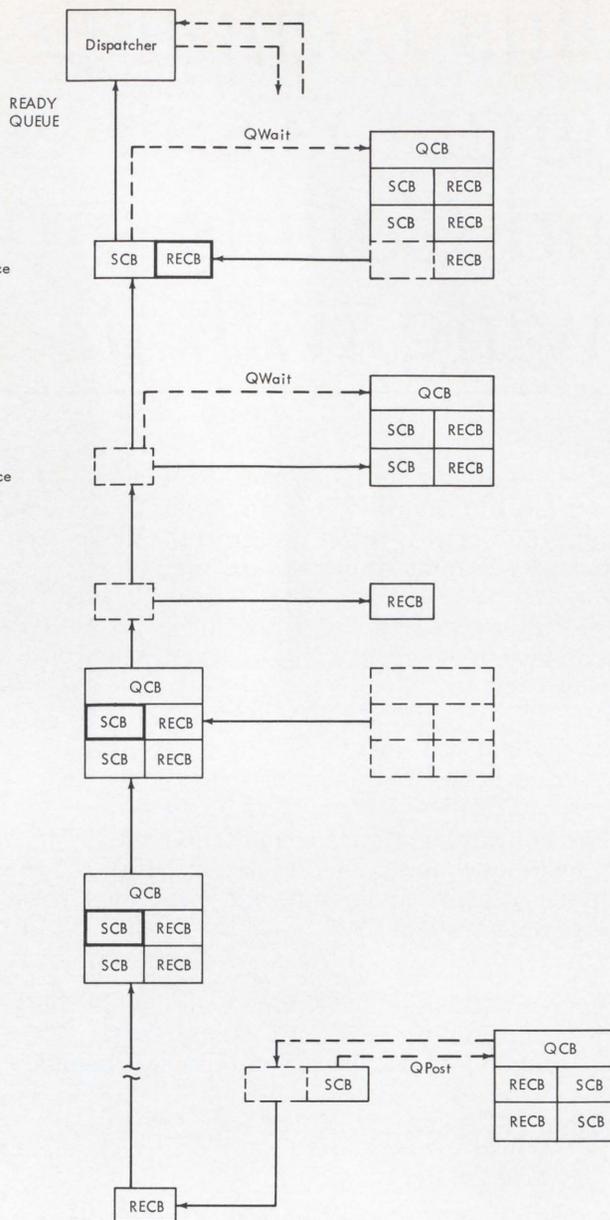
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### Legend

QCB - Queue Control Block  
SCB - Subtask Control Block  
RECB - Resource Element Control Block

Figure 1. Disposition of Ready Queue Elements

processing operation addresses only as far as the line adapter on a control unit. Many steps must be taken beyond that to operate the actual device at a desired terminal station. Polling and addressing, reading and writing responses, asking and answering "Who are You's"—all of these functions greatly extend the time and complicate the process of transmitting and receiving data. Many telecommunications devices were never intended to be attached to a computer; it is up to the systems program to make up the difference.

### More Man/Machine Interface Considerations—A new set of prob-

lems arises when the I/O device is actually being operated by a human. The program must be able to carry on a conversation and appear intelligent while doing it. Meanwhile, the man on the line is keying in data, making mistakes (some of which he recognizes), asking to cancel in the middle of a transaction on which processing has already begun, asking for something to be repeated that he lost because he was out of paper, and becoming irritated when the program hesitates in order to handle a higher-priority situation.

### Highly-Variable Data Structure and Volume—Tele-processing I/O is normally not done at the request of

a processing program; on the contrary, the program is usually executed at the request of the I/O. A read to a line is simply an invitation to whatever is out there to begin sending. When the start I/O is given, the program may not know whether there is anything to be read, how much is to be read, or the content or format of the data. In normal data processing, 80-character (card-size) blocks are often used. Tele-processing blocks may vary from eight to 32,000 characters. Also, instead of three or four types of data, as many as 50-80 may be received for processing.

It is the cumulative effect of all these factors which complicates the programming in a communications environment. The most important factors are the variable structure of the data and the greater number of I/O channels. The variable length of messages makes core allocation more complex. Sometimes, blocks must be divided between core and tape or disk. The large number of types of data encountered in Tele-processing requires as many different types of programs.

A large number of resources to be serviced, and a relatively small number of other resources with which to service them, makes it necessary for all resources to be shared. The solution is to break up the resources into the smallest practical resource units, and to dynamically allocate them as needed to the smallest practical work unit.

In order to achieve efficient movement of resources through the QTAM system, subtasks were created. A subtask controls the manipulation of a resource. Optimally, a subtask should require only a single resource in order to perform the unit of work for which it was created. A subtask waits for a resource, operates upon it, and passes it to the next subtask. Thus, the multiplication of resources strongly affects the tasking concept.

#### Programming Aids

The Queued Telecommunications Access Method provides many aids to the construction of a Tele-processing system: addressing, polling, dialing, answering, sending, receiving, buffering, routing, queuing,



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error detection and correction, header analysis and synthesis, logging, translation, etc. Here, however, we are primarily interested in the way in which these facilities are offered to guide the user in constructing a more efficient system.

QTAM is much more than an access method. The user first must construct a complete message-control program. Once this is done, he can proceed to write any number of message-processing programs, using the simple OPEN, GET, PUT, and CLOSE macro instructions as with any other access method. The message-control program is constructed through the use of environmental and procedural macro instructions. The process of using these macro instructions is more like using a high-level compiler language than using typical macro definitions. It is an extremely flexible language, including the possibility, but seldom the necessity, of direct assembler code. At the same time, it is structured in such a way as to lead the user step-by-step through the entire process.

The message-control program is really a generalized switching program: messages are switched from one communications line to another or from a line to a processing program; they are switched from one processing program to another, or from a program to a communications line. The operation of this message-control program is completely asynchronous to that of the processing programs. It continuously monitors the network, reading messages as they appear and writing them in disk queues. Output mes-

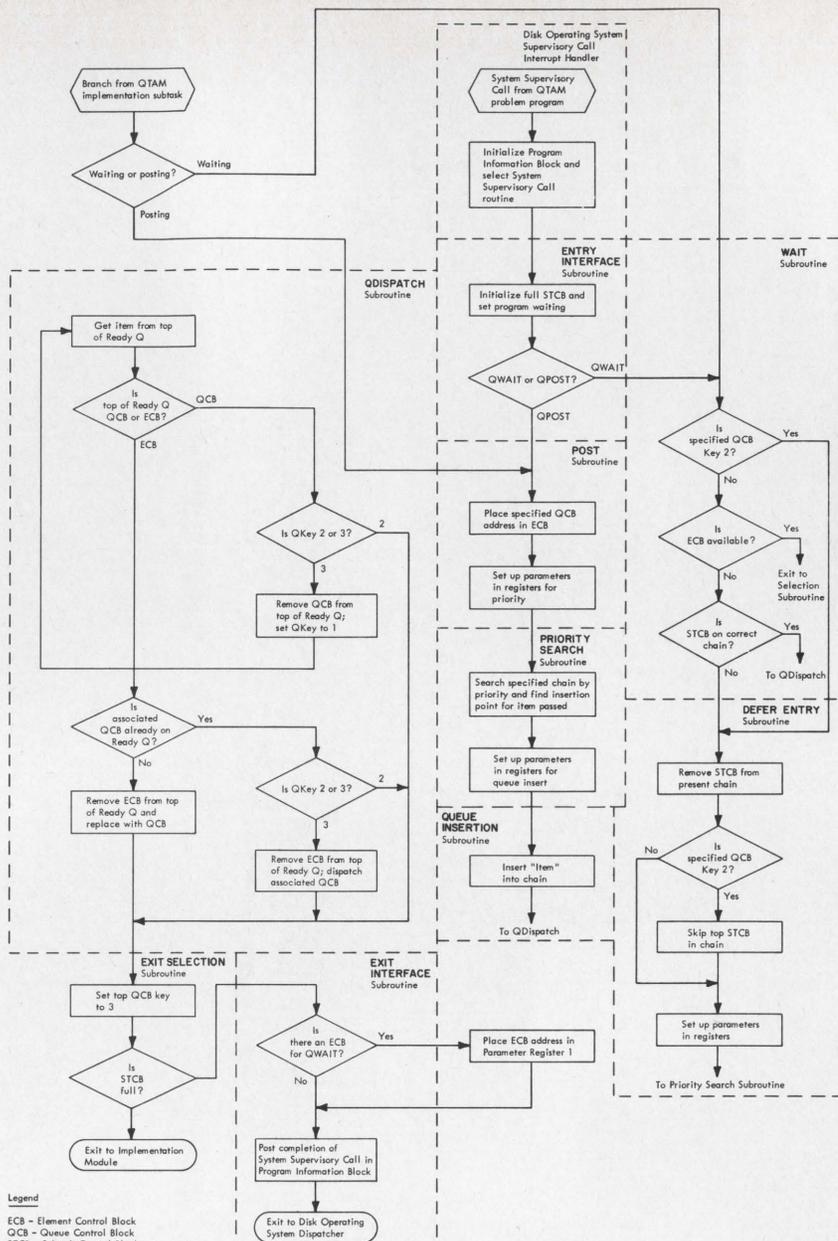


Figure 2. QTAM

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sages are taken from disk queues and sent out on the lines as the lines become available. Message-processing programs are loaded as necessary and transfer messages from and to disk (through message control).

Message control is run in the highest-priority partition; the message-processing program (or programs) in lower priority. The user is aware only of this relatively straightforward, 2-program structure. In order to understand the priority structure of QTAM, however, it is necessary to step outside of the operating system framework and look at QTAM as an independent, multi-tasking control program.

#### Resource Allocation

QTAM resource allocation is controlled by a set of routines executed as part of the operating system supervisors. These allocate resources and dispatch subtasks.

All resources (lines, buffers, and buffer-request blocks) are represented by Resource Element Control Blocks in core. A Resource Element Control Block can represent one type of element at one time, another at a different time. For example, an empty buffer assigned to receive a message is an entirely different type of resource than that same buffer later when it contains a message segment and is waiting to be written on disk.

All programs are organized into subtasks, each of which is represented by a Subtask Control Block. Most of the subtasks are permanently defined. For the most part, these are the functions involved in the actual control of the lines and the disk queues, and they are executed in supervisor state, disabled to interruptions. In addition to these, there are the problem-program subtasks created whenever the message-control program or one of the message-processing programs requests or passes a resource.

The key to the allocation and scheduling mechanism of QTAM is the structure through which a resource is allocated to a subtask—the Ready Queue. The nodes of the allocation and scheduling mechanism are Queue Control Blocks which queue both resources waiting to be operated upon and subtasks waiting

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for a particular type of resource. There is a Queue Control Block for each type of resource in the system.

Queue Control Blocks can be looked at as "nodes" of the system from two points of view, corresponding to the two different definitions of the word "node." First, each is a node in the sense of a knot which ties together two strings (a string of resource with a string of sub-tasks). It is also a node in the sense of a point where a moving process becomes still. As a resource is passed from one subtask to another (or, from another point of view, as a sub-task passes from one resource to another) it comes to a resting place on the Queue Control Block. If conditions in the system require it, resources and subtasks can be allowed to build up into queues chained to the Queue Control Block.

When a subtask is finished with a resource, it posts or chains the resource directly to the Ready Queue, in proper priority sequence. Thus, at any given moment, the Ready Queue consists of a chain of Queue Control Blocks and Resource Element Control Blocks arranged in a priority sequence. The position of all items on the Ready Queue is determined by the relative priorities of resource elements as they are passed to the queue. Generally speaking, the priority of a resource element is determined by the type of subtask to which it is being passed.

When a subtask requires another resource, it issues a QUEUE WAIT on the proper Queue Control Block. If the resource is available, control is returned to the requesting subtask immediately. If not, the Subtask Control Block for this subtask

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is chained to the Queue Control Block, control passes to the QTAM dispatcher, and the next item on the Ready Queue is examined. In those cases where more than one subtask may request the same resource, the Subtask Control Blocks may be chained to the Queue Control Blocks in priority sequence, as are the Resource Element Control Blocks.

A subtask requests the resources it requires for its execution from the appropriate Queue Control Block, executes its function, and then passes the resource to the proper Queue Control Block for the next function to be performed. The rate at which a subtask acquires resources is based on the availability of the resources and the priority of the subtask itself. The availability of resources is optimized by allocating only those resources required, and only when they are required.

A more subtle, difficult to describe factor that enters into the QTAM allocation mechanism is the capability to decide the actual priority of a resource dynamically, depending on the current status of the system. For example, a buffer-request block

which is "asking" for a buffer for a line operation is normally of lower priority than a buffer-request block "asking" for a buffer for a disk operation.

However, before posting a line buffer-request block to the Ready Queue, QTAM compares the length of the disk I/O request queue to the number of high-priority buffer requests. If there are more I/O requests than there are high-priority buffer requests, it is an indication that the priority of the line-buffer request can probably be raised without showing the disk operations.

The effect of all this is to shift the importance of different functions in the system. The tendency is to increase efficiency by allowing the system to decide at the time a resource becomes available how it is to be used. QTAM is self-regulating, allowing optimum resource utilization in a constantly-changing environment.

### Conclusions

The approach to allocation and scheduling described here, and demonstrated by the QTAM program, can perhaps be best put into perspective by examining the extent of dynamic allocation achieved in current IBM System/360 systems. In the basic programming systems, all allocation is static within a given job. With Disk Operating System and Operating System "Multi-Programming with Fixed Tasks," multi-jobbing, and allocation are static throughout a job step. Although these systems share processing time between the various jobs, this must not be confused with dynamic allocation. The assignment of relative priorities to these jobs (or rather

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the assignment of a job to a partition) determines the allocation of time throughout the job step. The dispatcher simply activates the job to which time was previously allocated.

Operating System "Multi-Programming with Variable Tasks" takes the next step, allowing multi-tasking at least with a region, with resources now being assigned to a region for the duration of a job step. Within that region, however, the resource can be given from one task to another and then back again. Thus a resource may be considered assigned to one of these "daughter" tasks only for the duration of that task's existence.

In QTAM, however, a resource is never, in a sense, statically assigned to a subtask but is passed to the subtask at the moment that the subtask is dispatched. When a subtask has finished operating on the resource, it can pass the resource on to the next subtask and—most significantly—the subtask can *ask* for another. Furthermore, when a resource becomes available, it can, in effect, ask for a subtask.

This last point is the essential difference between QTAM and other priority-scheduled control programs. By treating subtasks and resources in exactly the same way, by allocating and dispatching them with a single-queue management facility, it becomes possible to base the first level of priority on the resource itself, instead of on a physical partition or even on a task. Since all resources, including physical resources, subtasks, and time, are allocated by a single mechanism, it becomes possible for the first time to base allocation on:

- first, the availability and priority of resources;
- second, the priority of the task.

Most of the facilities provided by QTAM are peculiar to a Tele-processing environment. So too is the absolute requirement for such a high rate of change in resource allocation. However, a single mechanism of this type could be provided for an entire operating system. Such a system should allow a greater utilization of total system resources, with less overhead cost, than when allocation is performed through several different mechanisms. ■



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## NEW PRODUCTS

(Continued from page 6)

capability, and increasing the number of time sharing computers in the SDS product line to four.

The new Sigma 5 time sharing system is a lower priced version of the time sharing system available with the Sigma 7.

The new Sigma 5 Batch Time-Sharing software permits interactive time sharing for up to eight simultaneous users; at the same time the system runs batch problems written in FORTRAN, COBOL, or assembly language. Batch throughput is maintained at a high level in the time sharing Sigma 5 by dedicating primary system resources and significant percentages of time to batch jobs and assigning on-line users to specified time slices as their demands require.

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3. The Sigma 5 time sharing system is specifically intended for applications in which large general purpose scientific problems are solved in a batch mode; at the time a number of programmers and other users perform simultaneous time sharing.

4. Sigma 7, the largest system offered by SDS, can solve scientific oriented problems, perform business data processing jobs and real time tasks, while simultaneously providing conversational time sharing.

With the addition of the Sigma 5 time sharing configuration to the SDS line, SDS now offers a greater number of time sharing systems for a larger variety of applications than any other company.

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posit slips can be provided where direct employee deposits are made to a bank. Personnel record is provided which includes job classification and other personnel information.

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\* \* \*

A ten-minute color film describing the strides in computer tape technology which have enabled the development of a non-certified, yet guaranteed performance tape, has been announced by 3M Company.

Produced by 3M's Magnetic Products division, the film is shot on location in a modern data processing facility and the company's magnetic tape plant in Hutchinson, Minn. Included is a history of the evolution of computer tape and an extensive look at the quality control behind the new "Guaranteed Performance" product. Narration is by Peter Jennings (ABC News).

3M will provide the projection equipment and personnel for showings in individual data centers.

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\* \* \*

An unusually wide line of perforator tapes in the fanfold format has been announced by Robins Data Devices, Inc., subsidiary of Robins Industries Corp., College Point (Flushing), N. Y. 11356. Seventy-one types are listed.

The new fanfolds have application in data processing, communications, numerical control, photo-typesetting and computer functions. They are especially useful in short-run applications on data processing equipment and have advantages in storage because fanfolded tape can be filed more readily with original documents.

The perforator tapes come in paper, mylar and laminated materials, oiled, un-oiled, and in colors. They are also printed with directional arrows, or unprinted.

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\* \* \*

Arvey Corporation, Chicago, has added three new Mylar reinforced combinations to its present line of perforator tapes. Identified as R-V-CZ-64, .003", Mylar/foil/Mylar; R-V-CP-115, .004", paper/Mylar/paper; and R-V-CT-52D, .0028", metalized Mylar, the tapes are reported to offer improved performance for N/C applications.

The company states that it produces the most versatile range of perforator tapes for numerical control, data processing, computer programming and equipment testing. Tape thicknesses range from .0043" down to .0015". All standard colors, widths and thicknesses are available.

Tapes are also produced to custom specifications. Arvey tapes are opaque to both infrared and visible light and meet the most rigid requirements for photo-electric and electro-mechanical readers; offer exceptional dimensional stability and are sold in guaranteed continuous measured roll lengths without splices. Inspection and testing methods comply with MIL standards.

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# TROUBLE-TRAN PRESENTS XTRAN'S ADVENTURES IN FORTRAN

Send your ANSWER to the problems posed here in each issue to:

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**software age**

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You can also profit by submitting PROBLEMS for this feature. If your problem in FORTRAN programming is selected for use in this feature, you will receive \$25.00

#### Contest Rules:

1. USA Standard FORTRAN is assumed.
2. CDC-6000 FORTRAN and IBM System/360 FORTRAN IV (level H) are used in verifying answers.

The correct answer bearing the earliest postmark will net the reader submitting it \$25.00

The second correct answer with earliest postmark wins \$15.00



By GEORGE N. VASSILAKIS  
of TRW's Software and Computing Center

## PROBLEM OF THE MONTH

Mr. XTRAN was asked to zero-out, in the beginning of his main program, all the labeled COMMON storage he was using. He reasoned that, since the main program would always be loaded first and the loader would assign contiguous storage to all the blocks of COMMON storage, one DO loop would suffice.

So, here is what he did.

```

Main Program
COMMON/R/R(5)          10 R(J) = 0.
COMMON/X/X/X/Y/Y/Z    .
COMMON/W/W(10)        .
DO 10 J = 1,18          END
  
```

Will the DO loop zero-out all COMMON storage? Is the statement COMMON/X/X/X/Y/Y/Z a legitimate FORTRAN statement? If yes, what does it mean?

## ANSWER TO LAST MONTH'S PROBLEM

First, I would like to apologize for the mysterious appearance of the alphabetic character Ø in places where the numeric 0 (zero) should have been. The problem is that the typesetting is done by non-programmers; and, because of publication deadlines, I do not have the opportunity to proofread the final text.

In last month's problem, you were asked to complete the coding that would enable subroutine B to transfer to statement 100 in the middle of subroutine A without subroutine B using the RETURN or CALL statements.

The given coding was:

SUBROUTINE A	SUBROUTINE B
.	.
IF(1.GT.0) GØ TØ 10	.
100 WRITE(3,110)	.
110 FØRMAT(14H RIGHT YØU ARE)	.
RETURN	.
10 .	IF(1.LT.0) RETURN
CALL B	END
.	
END	

The key to this problem is to create a label 100 in COMMON storage and transfer to it from subroutine B. Here is one solution:

SUBROUTINE A	SUBROUTINE B
COMMON /M/M	COMMON /M/M
IF(1.GT.0) GØ TØ 10	10 IF(1.LT.0) ASSIGN 10
100 WRITE(3,110)	TØ M
110 FØRMAT(14H RIGHT YØU ARE)	IF(1.LT.0) GØ TØ 20
RETURN	GØ TØ M, (10)
10 ASSIGN 100 TØ M	20 RETURN
CALL B	END
RETURN	
END	

This problem worked on the IBM 7094 and the CDC-6500, but did not work on the IBM system/360. I would appreciate hearing from users of other systems.

Time and space do not permit me to go into all the details of why this problem did not work on the IBM 360; however, it has to do with the "base-displacement addressing approach" and the ability to relocate programs and data at load time.

P. S. Once again I would like to ask my readers if there is any interest in rotating problems with FOTRAN algorithms.

June Winners: 1st—Alfred E. Ricconi, Madison, Wisconsin; 2nd—Val Tareski, Urbana, Illinois.

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